

Design Parameters of Transformer

Chinmayi Satish Thakare

Final Year B.E. Electrical Engineering

Jawaharlal Darda of Engineering and Technology, Yavatmal, Maharashtra, India

cthakare002019@gmail.com

Abstract: Transformers are used to change ac voltage levels, as well as to provide galvanic isolation between circuits. Single and three phase transformers are extensively employed in the world's power distribution system. This chapter considers the design of single phase power transformers. It reviews the classic transformer equivalent circuit and also considers its use in steady state phase or analysis. The chapter focuses on single phase transformers. Single phase transformers are often classified as being either core type or shell type. The chapter discusses transformer performance considerations such as the calculation of transformer parameters, regulation, magnetizing current, operating point analysis, and inrush current, all in general terms. It also focuses on one specific class of transformer, develop an Magnetic Equivalent Circuit, and ultimately a design approach. Core loss is a significant contributor to overall transformer loss and dominates no load losses.

Keywords: Road hypnosis, Driver behavior, Safety warning, Monotonous city effect.

I. INTRODUCTION

A transformer transfers electric power from one circuit to another circuit without a change in frequency. It contains primary and secondary winding. The primary winding is connected to the main supply and secondary to the required circuit. In our project circuit, we have taken the design of low power (10 KVA) single phase 50 hertz power transformer as per our requirement in the project.

The transformer is basically of three types:

- Core Type
- Shell Type
- Toroidal

In core, type windings surround a part of the core whereas in shell type core surrounds windings. In the Core type, there are two main types namely E-I type and U-T type. In this transformer design, we used E-I core type. We chose E-I core type as the winding is much easier when compared to toroidal, but efficiency is very high (95%-96%). It is so because flux loss is very less in toroidal cores comparatively.

Example of core type transformer looks like :-



Fig.1: Three phase transformer(6 type core winding)

The transformers employed in the project are

- **Series transformer:** To provide the required boost or buck voltage and
- **Control transformer:** For sensing the output voltage and for power supply.

Design Formulas:

Here we take the reference of winding data on enameled copper wire table and dimensions of transformer stampings table to select input and output windings SWG and core of the transformer for given specifications.

The design procedure is followed assuming that the following specification of a transformer are given:-

- Secondary voltage (Vs)
- Secondary current (Is)
- Turns ratio (n2/n1)

From these given details we calculate Tongue width, stack height, core type, window area as follows:-

- Secondary Volt-Amps (SVA) = secondary voltage (Vs) * secondary current(Is)
- Primary Volt-Amps (PVA) = Secondary Volt-Amps (SVA) / 0.9 (assuming efficiency of the transformer as 90%)
- Primary voltage (Vp)= Secondary voltage(Vs)/ turns ratio(n2/n1)
- Primary current (Ip) = Primary Volt-Amps(PVA)/ Primary voltage(Vp)

The require cross-sectional area of the core is given by:-

- Core area (CA) = 1.15 * sqrt (Primary Volt-amps(PVA))
- Gross core area (GCA) = Core area(CA) * 1.1

The number of turns on the winding is decided by the ratio given as:- Turns per volt (Tpv) = 1/(4.44 * 10⁻⁴ * core area * frequency * flux density)bh

Winding data on Enameled copper wire

Max. Current Capacity (Amp.)	Turns/Sq. cm	SWG	Max. Current Capacity (Amp.)	Turns/Sq. cm	SWG
0.001	81248	50	0.1874	711	29
0.0015	62134	49	0.2219	609	28
0.0026	39706	48	0.2726	504	27
0.0041	27546	47	0.3284	415	26
0.0059	20223	46	0.4054	341	25
0.0079	14392	45	0.4906	286	24
0.0104	11457	44	0.5838	242	23
0.0131	9337	43	0.7945	176	22
0.0162	7755	42	1.0377	137	21
0.0197	6543	41	1.313	106	20
0.0233	5595	40	1.622	87.4	19
0.0274	4838	39	2.335	60.8	18
0.0365	3507	38	3.178	45.4	17
0.0469	2800	37	4.151	35.2	16
0.0586	2286	36	5.254	26.8	15
0.0715	1902	35	6.487	21.5	14
0.0858	1608	34	8.579	16.1	13

0.1013	1308	33
0.1182	1137	32
0.1364	997	31
0.1588	881	30

10.961	12.8	12
13.638	10.4	11
16.6	8.7	10

Dimension of Transformer stampings (Core table):

Type Number	Tongue Width (cm)	Window (Sq. cm)	Area
17	1.27	1.213	
12A	1.588	1.897	
74	1.748	2.284	
23	1.905	2.723	
30	2	3	
	1.588	3.329	
31	2.223	3.703	
10	1.588	4.439	
15	2.54	4.839	
33	2.8	5.88	
1	1.667	6.555	
14	2.54	6.555	
11	1.905	7.259	
34	1.588	7.529	
3	3.175	7.562	

Type Number	Tongue Width (cm)	Window (Sq. cm)	Area
9	2.223	7.865	
9A	2.223	7.865	
11A	1.905	9.072	
4A	3.335	10.284	
2	1.905	10.891	
16	3.81	10.891	
3	3.81	12.704	
4AX	2.383	13.039	
13	3.175	14.117	
75	2.54	15.324	
4	2.54	15.865	
7	5.08	18.969	
6	3.81	19.356	
35A	3.81	39.316	
8	5.08	49.803	

For operation on mains supply, the frequency is 50HZ, while the flux density can be taken as 1Wb/sq cm. for ordinary Steel stampings and 1.3Wb/sq cm for CRGO stampings, depending on the type to be used.

Hence

Primary turns (n1) = Turns per volt(Tpv) * Primary voltage(V1)

Secondary turns (n2) = Turns per volt(Tpv) * secondary voltage(V2) * 1.03 (Assume that there is 3% drop in transformer windings)

The width of the tongue of laminations is approximately given by:-

Tongue width (Tw) = Sqrt * (GCA)

Current density

It is the current carrying capacity of a wire per unit cross sectional area. It is expressed in units of Amp/ cm². The above mentioned wire table is for a continuous rating at current density of 200A/cm². For non-continuous or intermittent mode of operation of transformer one can choose a higher density up to 400A/cm² i.e., twice the normal density to economize the unit cost. It is opted as, the temperature rise for the intermittent operational cases are less for the continuous operational cases.

So depending on the current densities chosen we now calculate the values of primary and secondary currents that are to be searched in wire table for selecting SWG:-

n1a = Primary current (Ip) calculated / (current density/200)

n2a = Secondary current (Is) calculated / (current density/200)

For these values of primary and secondary currents we choose the corresponding SWG and Turns per sqcm from the wire table. Then we proceed to calculate as follows:-

Primary area(pa)= Primary turns(n1) / (Primary turns per sqcm)

Secondary area(sa)= Secondary turns(n2) / (Secondary turns per sqcm)

The total window area required for the core is given by:-

Total area (TA) = Primary area (pa) + Secondary area (sa)

Extra space required for the former and insulation may be taken as 30% extra space of what is required by the actual winding area. This value is approximate and may have to be modified, depending on the actual winding method.

Window area (Wacal) = Total area (TA) * 1.3

For the above calculated value of tongue width, we choose core number and window area from the core table ensuring that the window area chosen is greater than or equal to the Gross core area. If this condition is not satisfied we go for a higher tongue width ensuring the same condition with a corresponding decrease in the stack height so as to maintain approximately constant gross core area.

Thus we get available tongue width (Twavail) and window area ((avail)(aWa)) from the core table

Stack Height = Gross core area / Tongue width ((available) (atw)).

For commercially available former size purposes, we approximate stack height to tongue width ratio to the nearest following figures of 1.25, 1.5, 1.75. At the worst case we take the ratio equal to 2. However any ratio till 2 can be taken which would call for making ones own former.

If the ratio is greater than 2 we select a higher tongue width (aTw) ensuring all the conditions as above.

Stack height(ht) / tongue width(aTw) = (some ratio)

Modified stack height = Tongue width(aTw) * Nearest value of standard ratio

Modified Gross core area = Tongue width (aTw) * Modified stack height.

Same design procedure applies for control transformer, where in we need to ensure that stack height equals Tongue width.

Thus we find core number and stack height for the given specifications.

Designing a transformer using an example:

The given details are as follows:-

Sec. voltage(Vs) = 60V

Sec current(Is) = 4.44A

Turns per ratio (n2/n1) = 0.5

Now we have to calculations as follows:-

$$\begin{aligned} \text{Sec.Volt-Amps(SVA)} &= V_s * I_s \\ &= 60 * 4.44 \\ &= 266.4\text{VA} \end{aligned}$$

$$\begin{aligned} \text{Prim.Volt-Amps(PVA)} &= \text{SVA} / 0.9 \\ &= 296.00\text{VA} \end{aligned}$$

$$\begin{aligned} \text{Prim.Voltage (Vp)} &= \text{V}_2 / (n_2/n_1) \\ &= 60/0.5 \\ &= 120\text{V} \end{aligned}$$

$$\begin{aligned} \text{Prim.current (Ip)} &= \text{PVA}/\text{Vp} \\ &= 296.0/ 120 \\ &= 2.467\text{A} \end{aligned}$$

$$\begin{aligned} \text{Core Area(CA)} &= 1.15 * \text{sqrt(PVA)} \\ &= 1.15 * \text{sqrt}(296) \\ &= 19.785 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Gross core area(GCA)} &= CA * 1.1 \\ &= 19.785 * 1.1 \\ &= 21.76 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Turns per volt(Tpv)} &= 1 / (4.44 * 10^{-4} * CA * \text{frequency} * \text{Flux density}) \\ &= 1 / (4.44 * 10^{-4} * 19.785 * 50 * 1) \\ &= 2.272 \text{ turns per volt} \end{aligned}$$

$$\begin{aligned} \text{Prim.Turns(N1)} &= Tpv * Vp \\ &= 2.276 * 120 \\ &= 272.73 \text{ turns} \end{aligned}$$

$$\begin{aligned} \text{Sec.Turns(N2)} &= Tpv * Vs * 1.03 \\ &= 2.276 * 60 * 1.03 \\ &= 140.46 \text{ turns} \end{aligned}$$

$$\begin{aligned} \text{Tongue width(TW)} &= \text{Sqrt}*(\text{GCA}) \\ &= 4.690 \text{ cm} \end{aligned}$$

We are choosing the current density as 300A/cm², but the current density in the wire table is given for 200A/cm², then

$$\begin{aligned} \text{Primary current search value} &= Ip / (\text{current density}/200) \\ &= 2.467 / (300/200) \\ &= 1.644\text{A} \end{aligned}$$

$$\begin{aligned} \text{Secondary current search value} &= Is / (\text{current density}/200) \\ &= 4.44 / (300/200) \\ &= 2.96\text{A} \end{aligned}$$

For these values of primary and secondary currents we choose the corresponding SWG and Turns per sqcm from the wire table.

$$\text{SWG1}=19$$

$$\text{SWG2}=18$$

$$\text{Turn per sqcm of primary} = 87.4 \text{ cm}^2 \text{ turns per sqcm of secondary} = 60.8 \text{ cm}^2$$

$$\begin{aligned} \text{Primary area(pa)} &= n1 / \text{turns per sqcm(primary)} \\ &= 272.73 / 87.4 \\ &= 3.120 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Secondary area(sa)} &= n2 / \text{turns per sqcm(secondary)} \\ &= 140.46 / 60.8 \\ &= 2.310 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Total area(at)} &= pa + sa \\ &= 3.120 + 2.310 \\ &= 5.430 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Window area (Wa)} &= \text{total area} * 1.3 \\ &= 5.430 * 1.3 \\ &= 7.059 \text{ cm}^2 \end{aligned}$$

For the above calculated value of tongue width, we choose core number and window area from the core table ensuring that the window area chosen is greater than or equal to the Gross core area. If this condition is not satisfied we go for a higher tongue width ensuring the same condition with a corresponding decrease in the stack height so as to maintain approximately constant gross core area.

Thus we get available tongue width (T_{avail}) and window area ((_{avail})_aWa) from the core table:

$$\text{So tongue width available (atw)} = 3.81\text{cm}$$

$$\text{Window area available (awa)} = 10.891 \text{ cm}^2$$

$$\text{Core number} = 16$$

$$\begin{aligned} \text{Stack Height} &= \text{gca} / \text{atw} \\ &= 21.99 / 3.810 \\ &= 5.774\text{cm} \end{aligned}$$

For performance reasons, we approximate stack height to tongue width (aTw) ratio to the nearest following figures of 1.25, 1.5, and 1.75. At the worst case we take the ratio equal to 2.

If the ratio is greater than 2 we select a higher tongue width ensuring all the conditions as above.

$$\text{Stack height(ht) / tongue width(aTw)} = 5.774 / 3.81 = 1.516$$

$$\begin{aligned} \text{Modified stack height} &= \text{Tongue width(aTw)} * \text{Nearest value of standard ratio} \\ &= 3.810 * 1.516 = 5.715\text{cm} \end{aligned}$$

$$\begin{aligned} \text{Modified Gross core area} &= \text{Tongue width (aTw)} * \text{Modified stack height} \\ &= 3.810 * 5.715 \\ &= 21.774 \text{ cm}^2 \end{aligned}$$

Thus we find core number and stack height for the given specifications.

Design of a small control transformer with example:

The given details are as follows:-

$$\text{Sec. voltage}(V_s) = 18\text{V}$$

$$\text{Sec current}(I_s) = 0.3\text{A}$$

$$\text{Turns per ratio } (n_2/n_1) = 1$$

Now we have to calculations as follows:-

$$\begin{aligned} \text{Sec.Volt-Amps(SVA)} &= V_s * I_s \\ &= 18 * 0.3 \\ &= 5.4\text{VA} \end{aligned}$$

$$\begin{aligned} \text{Prim.Volt-Amps(PVA)} &= \text{SVA} / 0.9 \\ &= 5.4 / 0.9 \\ &= 6\text{VA} \end{aligned}$$

$$\begin{aligned} \text{Prim. Voltage } (V_p) &= V_2 / (n_2/n_1) \\ &= 18/1 \\ &= 18\text{V} \end{aligned}$$

$$\begin{aligned} \text{Prim. current } (I_p) &= \text{PVA}/V_p \\ &= 6 / 18 \\ &= 0.333\text{A} \end{aligned}$$

$$\begin{aligned} \text{Core Area(CA)} &= 1.15 * \text{sqrt(PVA)} \\ &= 1.15 * \text{sqrt}(6) \\ &= 2.822 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Cross core area(GCA)} &= \text{CA} * 1.1 \\ &= 2.822 * 1.1 \\ &= 3.132 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Turns per volt}(T_{pv}) &= 1 / (4.44 * 10^{-4} * \text{CA} * \text{frequency} * \text{Flux density}) \\ &= 1 / (4.44 * 10^{-4} * 2.822 * 50 * 1) \\ &= 15.963 \text{ turns per volt} \end{aligned}$$

$$\begin{aligned} \text{Prim. Turns}(N_1) &= T_{pv} * V_p \\ &= 15.963 * 18 \\ &= 287.337 \text{ turns} \end{aligned}$$

$$\begin{aligned} \text{Sec.Turns}(N_2) &= T_{pv} * V_s * 1.03 \\ &= 15.963 * 60 * 1.03 \\ &= 295.957 \text{ turns} \end{aligned}$$

$$\begin{aligned} \text{Tongue width}(TW) &= \text{sqrt}*(\text{GCA}) \\ &= \text{sqrt} * (3.132) \\ &= 1.770 \text{ cm} \end{aligned}$$

We are choosing the current density as 200A/cm², but the current density in the wire table is given for 200A/cm², then

$$\begin{aligned} \text{Primary current search value} &= I_p / (\text{current density}/200) \\ &= 0.333 / (200/200) = 0.333\text{A} \end{aligned}$$

$$\begin{aligned} \text{Secondary current search value} &= I_s / (\text{current density}/200) \\ &= 0.3 / (200/200) \\ &= 0.3\text{A} \end{aligned}$$

For these values of primary and secondary currents we choose the corresponding SWG and Turns per Sq. cm from the wire table.

$$\text{SWG1}=26$$

$$\text{SWG2}=27$$

$$\text{Turn per Sq. cm of primary} = 415 \text{ turns}$$

$$\text{Turns per Sq. cm of secondary} = 504 \text{ turns}$$

$$\begin{aligned} \text{Primary area}(p_a) &= n_1 / \text{turns per sqcm(primary)} \\ &= 287.337 / 415 \\ &= 0.692 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Secondary area}(s_a) &= n_2 / \text{turns per sqcm(secondary)} \\ &= 295.957 / 504 \\ &= 0.587 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Total area}(a_t) &= p_a + s_a \\ &= 0.692 + 0.587 \\ &= 1.280 \text{ cm}^2 \end{aligned}$$

$$\begin{aligned} \text{Window area } (W_a) &= \text{total area} * 1.3 \\ &= 1.280 * 1.3 \\ &= 1.663 \text{ cm}^2 \end{aligned}$$

For the above calculated value of tongue width, we choose core number and window area from the core table ensuring that the window area chosen is greater than or equal to the Gross core area. If this condition is not satisfied we go for a higher tongue width ensuring the same condition with a corresponding decrease in the stack height so as to maintain approximately constant gross core area.

Thus we get available tongue width (T_{avail}) and window area ($(a_{avail})(a_{W_a})$) from the core table

$$\text{So tongue width available } (a_{tw}) = 1.905\text{cm}$$

$$\text{Window area available } (a_{wa}) = 18.969 \text{ cm}^2$$

$$\text{Core number} = 23$$

$$\begin{aligned} \text{Stack Height} &= gca / a_{tw} \\ &= 3.132 / 1.905 \\ &= 1.905\text{cm} \end{aligned}$$

Hence the control transformer is designed.

II. CONCLUSION

A procedure for the optimal transformer. A transformer is a passive electrical device that can change the voltage in an alternating current (AC) electric circuit. Transformers are used to increase or decrease the operating voltage levels between circuits.

REFERENCES

- [1]. Lowdon, E., Practical Transformer Design Handbook, McGraw-Hill, Inc., 2nd edition, 1989.
- [2]. McLyman, W.T., Transformer and Inductor Design Handbook, Dekker, New York, USA, 3rd edition, 2004.
- [3]. Rubaai, A., "Computer aided instruction of power transformer design in the undergraduate power engineering class", IEEE Trans. on Power Systems, Aug 94, v. 9, No. 3, pp. 1174-1181.
- [4]. H.L. Garbarino, "Some properties of the optimum power transformer design," Power Apparatus and Systems, Part III. Transactions of the American Institute of Electrical Engineers, vol.73, no.1, pp. 675-682,Jan. 1954.
- [5]. T.H. Putman, "Economics and power transformer design," IEEE Transactions on Power Apparatus and Systems, vol.82, no.69, pp.1018-1023, Dec. 1963.